



**RM-7849**

**B. E. IV (Sem. VIII) (Mech.) Examination**

**May / June – 2010**

**Design of Heat Exchangers**

Time : 3 Hours]

[Total Marks : 100

**Instructions :**

(1)

नीचे दशावलि निशानीवाणी विगतो उत्तरवही पर अवश्य लभवी. Fillup strictly the details of signs on your answer book.	Seat No. :
Name of the Examination :	<input type="text"/>
<input type="checkbox"/> B. E. 4 (Sem. 8) (Mech.)	<input type="text"/>
Name of the Subject :	<input type="text"/>
<input type="checkbox"/> Design of Heat Exchangers	<input type="text"/>
Subject Code No. : <input type="text"/> 7 <input type="text"/> 8 <input type="text"/> 4 <input type="text"/> 9	<input type="text"/>
Section No. (1, 2,.....) : <input type="text"/> 1&2	<input type="text"/>
	Student's Signature

- (2) Answer **all** questions.
- (3) Use **separate** answer book for each section.
- (4) Figures to the **right** indicates full marks.
- (5) Use of design of heat exchanger data book is permitted.
- (6) Assume suitable data, if **necessary**.

**SECTION – I**

- Q-1 Explain giving the precise reasons whether the following 10 statements are true or false:
- (1) In pull through tube bundles pressure drop on the shell side is reduced substantially by the leakage and by pass streams
  - (2) NTU values for most heat exchangers are limited to 5
  - (3) The square lay out is more effective in heat transfer than the triangular layout of tubes.
  - (4) For flow over fin tubes, the entrance and exit pressure loss coefficients are neglected
  - (5) Plate heat exchangers are widely used in milk pasteurizing
- Q-2
- (1) Draw single, double and triple segmented baffles. 10
  - (2) Draw Tinker's shell side flow model.

Q-3 **Attempt any two**

30

- (a) Consider the following data to design a water cooled shell and tube Freon condenser for the given heat duty:

Cooling load of the condenser	125 kW
Refrigerant	R-22
	Condensing temperature, 37°C in tube condensation
Coolant	City water
	Inlet temperature, 18°C
	Outlet temperature, 26°C
Heat transfer matrix	Mean pressure, 0.4 Mpa ¾ in OD, 20 BWG Brass tube
Value for shell and tube condenser are	
Np – 1 tube pass	
Ds = 0387 m	

Nt = 137 tubes

P<sub>T</sub> = 1" square pitch

Properties of shell side coolant fluid

T<sub>c1</sub> = 18°C

T<sub>c2</sub> = 26°C

D<sub>o</sub> = 0.75 in = 0.01905 m

Properties at saturation temperature

P<sub>sat</sub> = 14.17 bar

V<sub>l</sub> = 8.734 × 10<sup>-4</sup> m<sup>3</sup>/kg

μ<sub>l</sub> = 0.082 Pa-s

i<sub>fg</sub> = 169 kJ/kg

C<sub>pl</sub> = 1.305 kJ/kg-K

V<sub>g</sub> = 0.01643 m<sup>3</sup>/kg

μ<sub>g</sub> = 0.0000139 Pa-s

Pr = 2.96

Use following correlations

Shell side

$$\frac{h_o \cdot D_e}{k} = 0.35 \cdot Re_s^{0.55} \cdot Pr_s^{(1/3)} \cdot \left[ \frac{\mu_b}{\mu_w} \right]^{0.14}$$

Tube side :

$$h_{TP} = 0.05 \cdot Re_{eq}^{0.8} \cdot Pr^{(1/3)} \cdot \frac{k_L}{d_i}$$

Where

$$Re_{eq} = Re_v \cdot \frac{\mu_v}{\mu_L} \cdot \left[ \frac{\rho_L}{\rho_v} \right]^{0.5} + Re_L$$

Determine overall heat transfer coefficient, LMTD, heat transfer surface area and length of tube.

- (b) A split backing ring floating head type heat exchanger is proposed for the following process conditions. Verify whether the proposed design will meet the process requirement or not?

Tube OD = 19.05 mm	Overall tube length = 5 m
Tube ID = 14.83 mm	Effective tube length = 4.764 m
Pitch = 25.4 mm $\times$ 30°	No of shells = 1
No of tubes in shell = 744	No of velocity head lost in shell side nozzle = 4
No of tube pass = 4	No of velocity head lost in tube side nozzle = 1.8
Shell side nozzle ID = 254.5 mm	Tube side nozzle ID = 202.7
Shell ID = 889 mm	Correction factor for MTD = 0.92
Central baffle spacing = 275 mm	End baffle spacing = 550 mm
No of baffles = 14	

Use appropriate correlations for tube side from the data book

Item	Tube-side	Shell-side	Unit
Fluid name	Water	Oil	-----

Flow rate	45	63.77	Kg/s
Inlet temp	21	102	C
Outlet temp	49	64	C
Cp	4.187	2.177	kJ/kg-K
$\mu$	0.00072	0.00189	N-s/m <sup>2</sup>
K	0.64	0122	W/m-K
$\rho$	995	786.4	Kg/m <sup>3</sup>
Pr	4.8	33.73	-----
Fouling factor	0.00026	0.000018	M <sup>2</sup> -K/W
Max.Pr loss	50000	70000	Pa
Wall resistance	0.00004		M <sup>2</sup> -K/W

- (c) Using the lobo-Evans method, calculate the fuel required in a furnace, having the following characteristics:

Heat transfer in average radiant section – 325 W/m<sup>2</sup>

Dimension of combustion chamber: 4.5 $\times$ 9 $\times$ 12 m

Tube centre to centre spacing: 2.5 cm

Tube OD: 12 cm

Number of tubes arranged in single row: 90

Circumferential tube surface: 450 m<sup>2</sup>

Total wall area (At): 400 m<sup>2</sup>

Fuel oil atomization medium : 0.14 kg steam/kg oil

Heating value of fuel (LHV) : 40160 kJ/kg

Excess air : 26%

Estimated tube temperature: 550°C

Partial pressure of CO<sub>2</sub>:0.1084

Partial pressure of H<sub>2</sub>O: 0.1248

## SECTION – II

- Q-4 (a) Explain various regimes of forced convection boiling inside a vertical tube subjected to uniform wall temperature. 05
- (b) Hot oil is to be cooled in a double tube counter flow heat exchanger. The copper inner tube has a diameter of 2cm and negligible thickness. The inner diameter of outer tube is 3cm. Water flows through the copper tube at the flow rate of 0.5kg/s, and the oil passes through outer tube at a flow rate of 0.8kg/s. Temperature of water and oil are 45°C and 80°C, respectively, Calculate the overall heat transfer coefficient. 10

Properties of water at 45 °C

$$\rho = 990 \text{ kg/m}^3$$

$$\text{Pr} = 3.91$$

$$k = 0.637 \text{ W/m}^\circ\text{C}$$

$$\nu = 0.602326 \times 10^{-6} \text{ m}^2/\text{s}$$

Properties of oil at 80°C

$$\rho = 852 \text{ kg/m}^3$$

$$\text{Pr} = 490$$

$$k = 0.138 \text{ W/m}^\circ\text{C}$$

$$\nu = 37.5 \times 10^{-6} \text{ m}^2/\text{s}$$

- Q-5 (a) Explain various regimes of forced convection boiling inside a vertical tube subjected to uniform wall temperature. 05
- (b) Saturated steam at atmospheric pressure condenses on 2 m high and 3 m wide vertical plate that is maintained at 80°C by circulating water through the other side. Determine the rate of heat transfer by condensation to the plate and the rate at which the condensate drips off the plate at the bottom. 10

The properties of water at 100°C are

$$h_{fg} = 2257 \times 10^3 \text{ J/kg}$$

$$\rho_v = 0.6 \text{ kg/m}^3$$

The properties of water at the film temperature are

$$\rho_l = 965.3 \text{ kg/m}^3$$

$$C_{p_l} = 4206 \text{ J/kg}^\circ\text{C}$$

$$\mu_l = 0.315 \times 10^{-3} \text{ kg m/s}$$

$$k_l = 0.675 \text{ W/m}^\circ\text{C}$$

$$\nu_l = 0.326 \times 10^{-6} \text{ m}^2/\text{s}$$

OR

- (b) A cross flow heat exchanger is used for heat transfer between air and water. Both fluids are remaining unmixed. It is having heat transfer area of  $8.4\text{m}^2$ . Air enters at  $15^\circ\text{C}$  and its mass flow rate is  $2\text{ kg/s}$ , while water enters at  $90^\circ\text{C}$  and its mass flow rate is  $0.25\text{ kg/s}$ . Specific heat of air is  $1005\text{ J/kg}^\circ\text{C}$  and that of water is  $4180\text{ J/kg}^\circ\text{C}$ . The overall heat transfer coefficient is  $250\text{ W/m}^2\text{C}$ . Calculate the exit temperature of air and water as well as the total heat transfer rate. 10

- Q-6 (a) Answer the following 06
1. Compare Compact Heat Exchanger and Shell and Tube Heat Exchanger.
  2. Why dropwise condensation is more favorable than filmwise condensation?
  3. What are the limitations of LMTD method in heat exchanger?
- (b) It is required to size the compact heat exchanger based on the following data for gas to air compact heat exchanger 14

Fluid	Air	Gas
Entry temperature	$175^\circ\text{C}$	$429^\circ\text{C}$
Mass flow rate	$24.31\text{kg/s}$	$24.69\text{kg/s}$
A	$400\text{m}^2/\text{m}^3$	$574\text{m}^2/\text{m}^3$
B	256	367
Fin type	Louvered plate fin	Plain plate fin
Fin Pitch	$2.38\text{ fins/cm}$	$4.37\text{ fin/cm}$
Fin length	$0.9525\text{ cm}$	-
Hydraulic radius	$1.112\text{mm}$	$0.771\text{mm}$
Hydraulic diameter	$4.448\text{mm}$	$3.084\text{mm}$
Fin effectiveness	0.786	0.877
Inlet pressure of fluid	$1.02\text{bar}$	$1.02\text{bar}$
Effectiveness of heat exchanger	75%	
Physical properties		
Viscosity	$\mu_a = 28.52 \times 10^{-6}\text{ kg/(m - s)}$	$30.17 \times 10^{-6}\text{ kg/(m - s)}$
P	$1.996\text{ kg/m}^3$	$10000\text{ kg/m}^3$
$C_p$	$1037\text{ J/kg}^\circ\text{C}$	$1049\text{ J/kg}^\circ\text{C}$
Pr	0.67	0.67

	Air Side			Gas Side	
Re	j	F	Re	J	F
4000	0.00738	0.0375	1500	0.00444	0.0149
4030	0.00736	0.0374	1365	0.00456	0.0158
4060	0.00734	0.0373	1200	0.00471	0.0169

Calculate the core dimensions of the heat exchanger.

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